



WET END OPTIMIZATION

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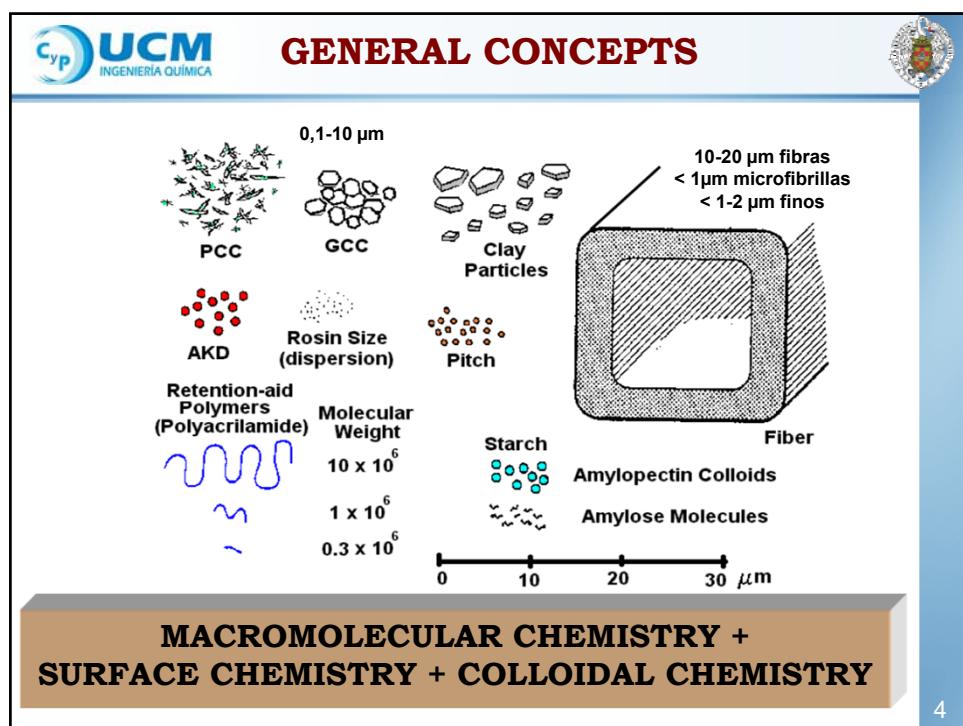
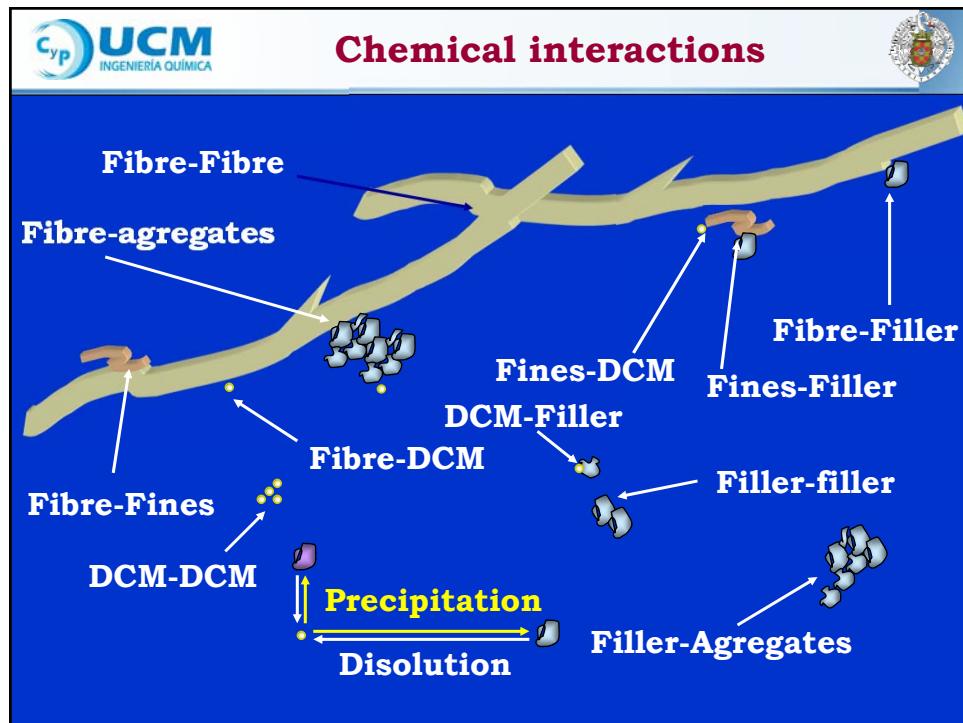


Content

- How to improve the effectiveness of papermaking chemicals.
- Balance between retention and drainage.
- Integration of water and retention system management
- On-line wet end control.
- Wet-end audit: Case studies.

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2





- When colloids are in a polar medium, they develop a surface charge:
 - Repulsion of particles
 - Attraction of counter-ions
- This, in addition to their tendency to mix due to thermal movements accounts for the formation of the electrostatic double layer.

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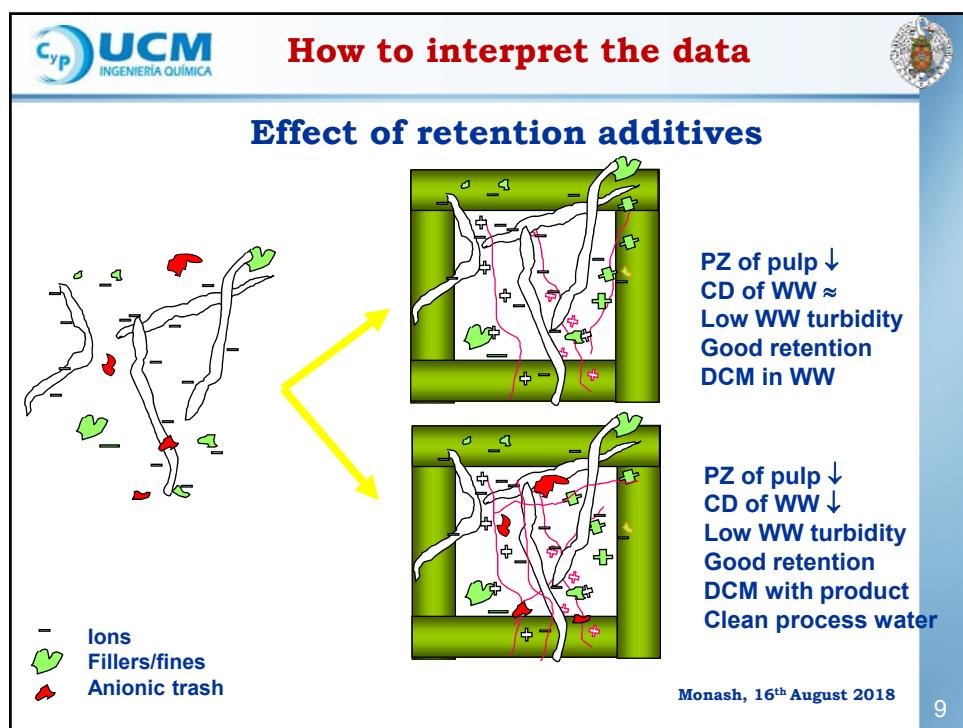
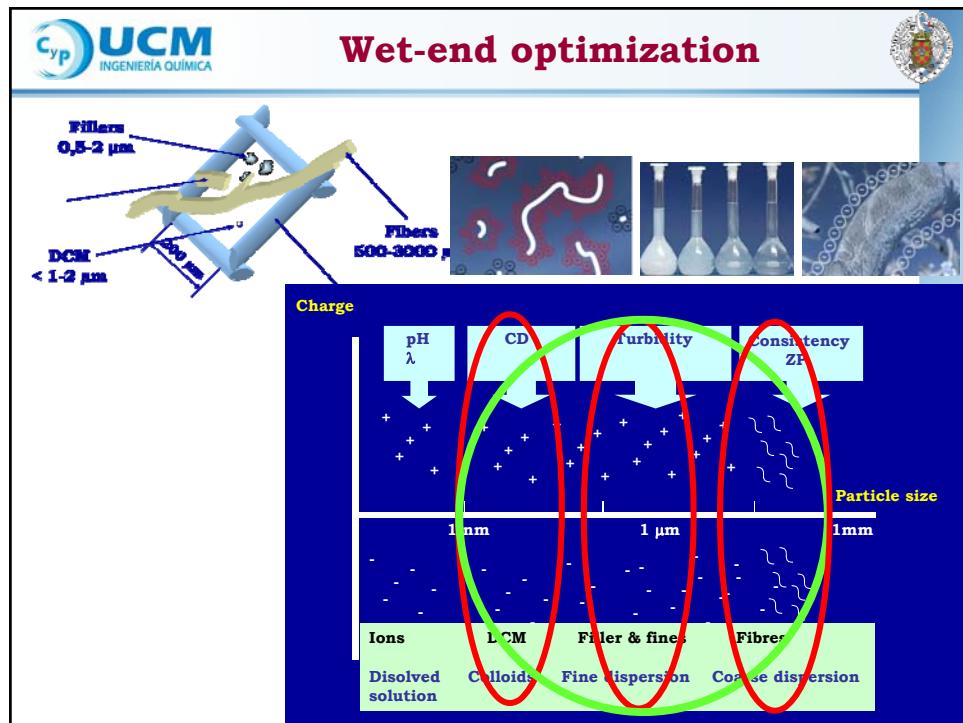
6



- It is based on the electrostatic double layer and stream flow theories.
- There is an important relation between the ZP and the stability of colloids.
- There is a correlation between ZP and electrokinetic parameters.
- If one of the phases moves tangentially in respect to the other, electrokinetic effects can be observed.

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7



Wet-end optimization



Traditional techniques:

- Based on electric properties
→ overdosification
- Conditions ≠ real process



Required techniques:

- Based on particle size changes
- On real time and on line

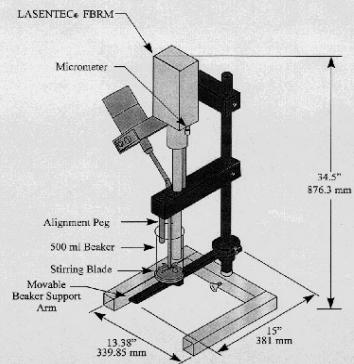


OBJECTIVES:

- Study of flocculation mechanisms and floc properties
- Wet end optimization



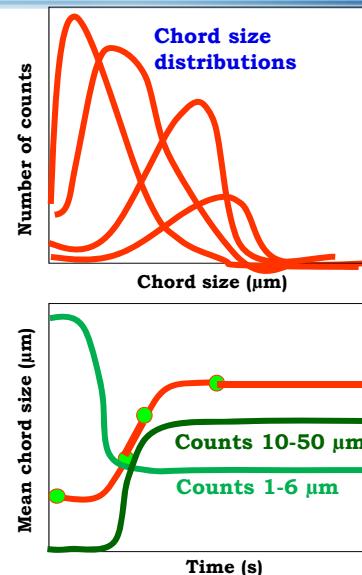
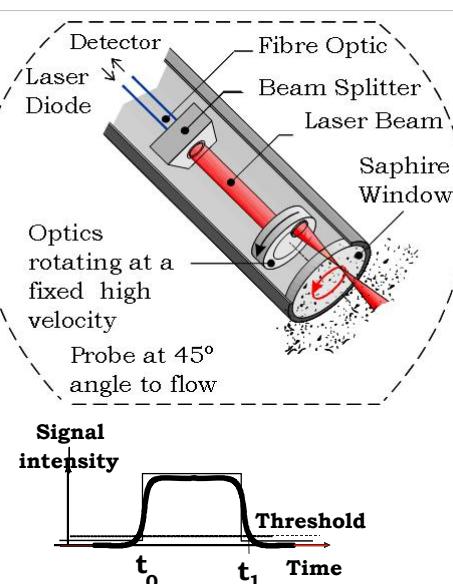
LASENTEC® STANDARD LAB PROBE
IN FIXED BEAKER STAND



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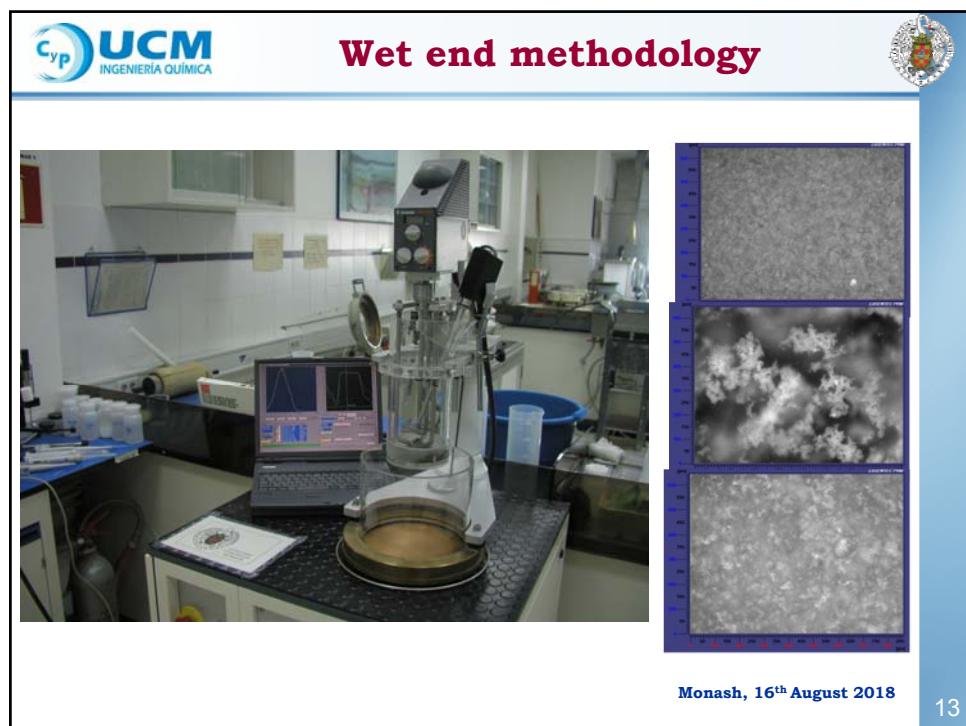
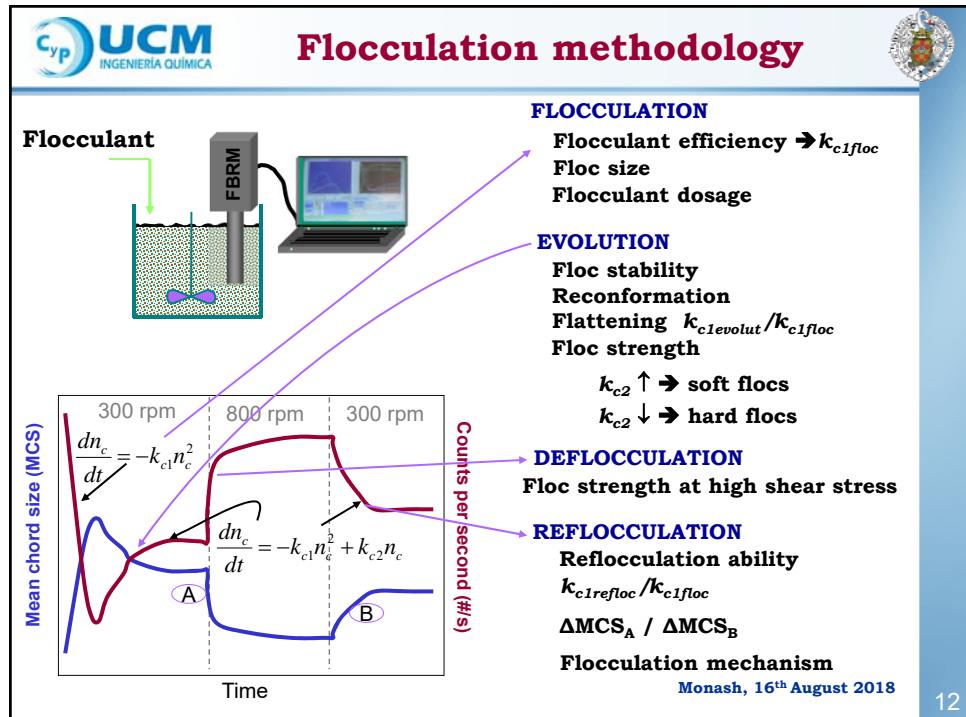
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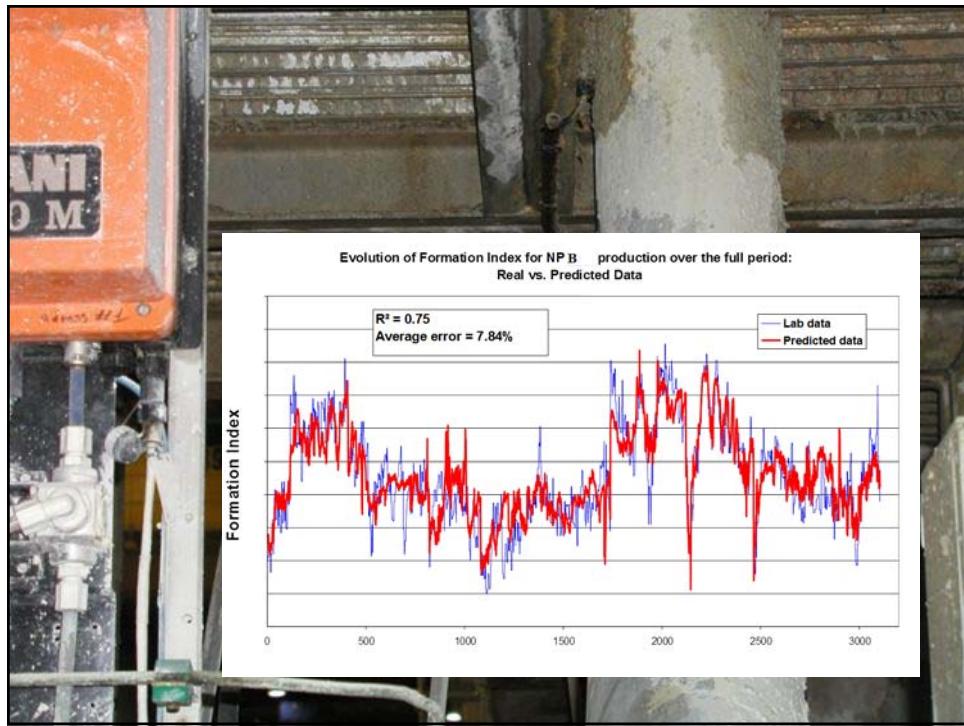
FBRM



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11





UCM INGENIERÍA QUÍMICA

FBRM methodology

1994 Method to optimize the polymer dosage for flocculation using the particle size analyzer (FBRM). Blanco et al. 1994, PhD thesis U.C.M

Influence of closed system on chemical flocculation" Towards the Closed System-Threats and Opportunities. Blanco, PIRA International. Leatherhead, Inglaterra. 1 March 1994.

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Influence of salt on the interaction of polymers with the different pulp fractions". TAPPI Papermakers Conference. San Francisco, 24 de abril de 1994.

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Flocculation-deflocculation-reflocculation kinetics and floc properties. Flocculation of DCM Blanco et al., 2002, Tappi J. 1(10):14; Blanco et al. 2002; CJChE. 80(4):734.

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15

FBRM methodology



- 2003** Flocculation of fillers, mechanisms Fuente et al. 2003, Pap. Technol. 44(8):41; Blanco et al. 2005, Ind. Eng. Chem. Res. 44(24):9105 Fuente et al. 2005, Ind. Eng. Chem. Res. 44(15):5616).
- Flocculation in fiber-cement industry Negro et al., 2005, Cem. Concr. Res. 35:2095).
- 2004** Flocculation mechanism induced by PEO/PFR dual system (Negro et al. 2005, AIChE J. 51(3):1022).
- Optimization of the fiber-cement flocculation process with FBRM Negro et al. 2005, Composites A. 36(12):1617; Negro et al. 2006, Cem. Concr. Comp. 28(1):90; Negro et al. 2006, Chem. Eng. Sci. 61:2522
- 2005** FBRM on line to predict fiber-cement product properties Negro et al. 2006, Ind. Eng. Chem. Res. 45(1):197).
- Predicition of paper properties based on wet end parameters Blanco et al. 2006 Int. RTA Users' Conf., Feb., Barcelona, Spain Control Systems 2006, Tampere, Finland); Blanco et al, 2009, Math. Comp. Model. Dyn. 15(5):453
- 2006** Comparative study of wet-end additives Cadotte et al. 2007, Can. J. Chem. Eng. 85(2):240; Hu and Hu, 2007, Res. Prog. Pap. Ind. Bioref., 1-3:1601.

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16

FBRM methodology



- 2008** Separation of contaminants from deinking process water by dissolved air flotation: effect of flocculant charge density/ Miranda et al. 2008, Sep. Sci. Technol, 43(14):3732
- 2009** Effect of fibre morphology on flocculation of fibre-cement suspensions. Tonoli et al. 2009, Cem. Conc. Res., 39(11):1017
- Influence of water quality in the efficiency of retention aids systems for the paper industry Ordoñez et al. 2009, Ind. Eng. Chem. Res, 48:10247.
- Influence of cationic starch adsorption on fiber flocculation Zakrajsek et al. 2009, Chem. Eng. Technol. 33(8):1259.
- Polymeric Branched Flocculant on Flocculation in the Papermaking Blanco et al. 2009, Ind. Eng. Chem. Res 48(10):4826
- 2009** Flocculation efficiency of chitosan for papermaking applications Nicu et al. 2013, Bioresources 8(1):768; Miranda et al. 2013 Chem. Eng. J., 231:304
- Silica removal from newsprint mill effluents. Latour et al. CEJ 230:522-531
- 2013** Influence of SS on silica removal by coagulation with aluminum salts. Miranda et al. CCT 49,497-510
- 2015** Optimization of silica removal with magnesium chloride in papermaking effluents: mechanistic and kinetic studies. ESPR 23(4) 3707-3717.
- Efficiency of polyaluminum nitrate sulphate-polyamine hybrid coagulants for silica removal. Desalin. Wat. Treat. 57(38), 17973-17984.

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17

FBRM methodology 2016 -1018

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Evaluation of the flocculation and reflocculation performance of a system with calcium carbonate, cationic acrylamide co-polymers, and bentonite microparticles. Antunes et al. Ind. Eng. Chem. Res. 54(1), 198-206
Efficiency of chitosan and their combination with bentonite as retention aids in papermaking. Bioresources 11(4), 10448-10468.

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Experimental and modelling approach to the catalytic coproduction of glycerol carbonate and ethylene glycol as a means to valorize glycerol. J. Taiwan Inst. Chem. Eng. 63, 89-100.

Estimation of Chlamydomonas reinhardtii biomass concentration from chord length distribution data. J. Applied Phycology 28(4) 2315-2322.
Laser reflectance measurement for the online monitoring of Chlorella Sorokiniana biomass concentration. J. of Biotechnology, 243(2), 10-15. **Estimation fractal dimension of microalgal flocs through confocal laser scanning microscopy and computer modelling.** Algal Research-Biomass Biofuels and Bioproducts 28 (2017), 74-79

Effect of polyelectrolyte morphology and adsorption on the mechanism of nanocellulose flocculation. Raj et al. J. Coll. Interf. Sci. 481, 158-167
Microfibrillated cellulose as a model for soft colloid flocculation with polyelectrolytes. Raj et al. Colloids Surf. A - Physicochemical and Engineering Aspects, 516, 325-335.
Synergies between cellulose nanofibers and retention additives to improve recycled paper properties and the drainage process. Cellulose, 24(7), 2987-3000.
Interactions between cellulose nanofibers and retention systems in flocculation of recycled fibers. Cellulose 24(2) (2017), 677-692

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18

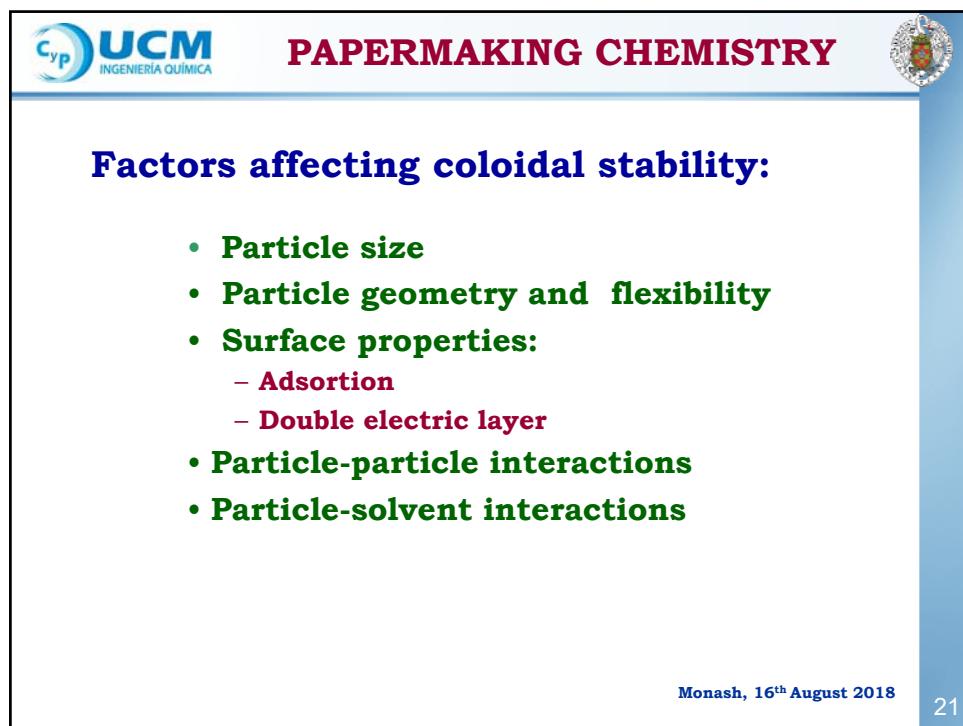
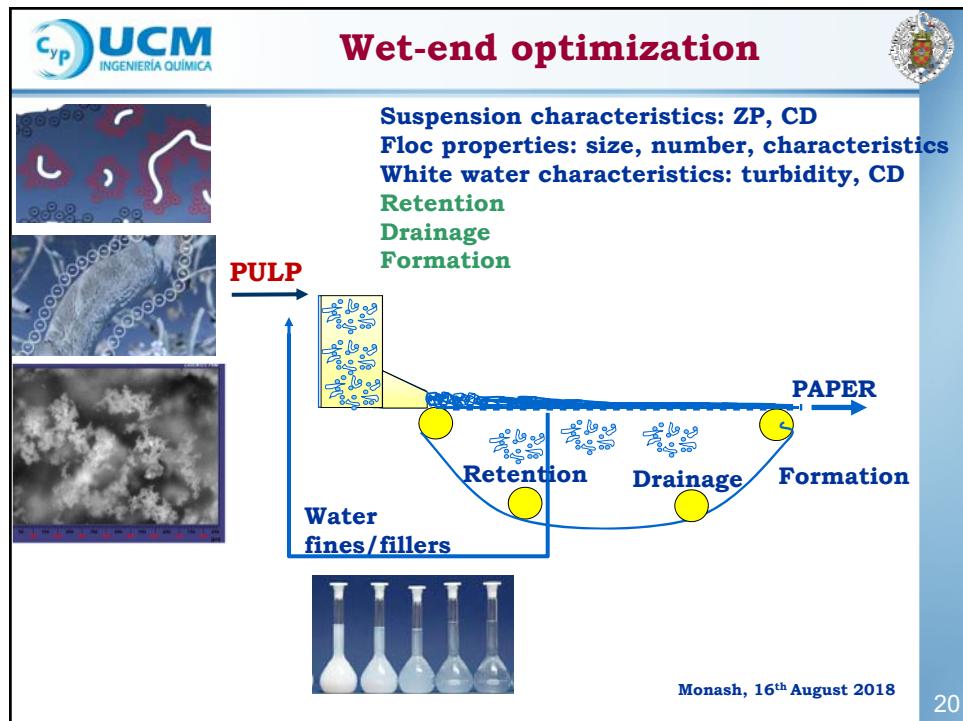
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19





Forces involved between particles

- Repulsive forces:

- Electrostatic
- Born

- Attractive forces:

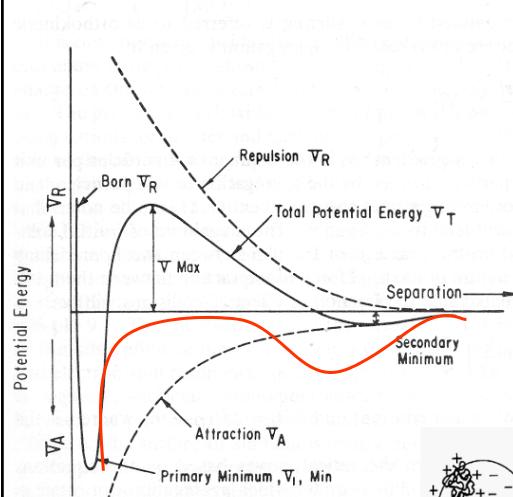
- Van der Waal forces
- Lewis base-Lewis acid interactions

- Brownian movement

- Steric stabilisation

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22



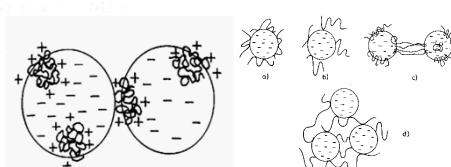
FLOCCULATION $\rightarrow F_A > F_R$

↓ Repulsive forces
→ ξ reduction

Attractive forces
↑ → Chemical interactions

FLOCCULATION MECHANISMS

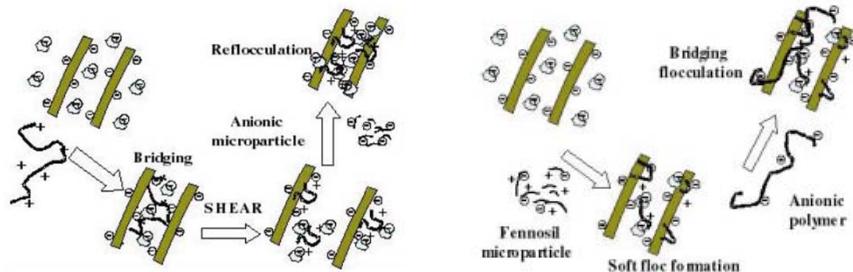
- Neutralization
- Patching
- Bridging
- Complex



23



- Single polymers: PEI, PA (patch) o PAM (bridges).
- Dual systems: PEI + PAM → patch + bridges.
- 2-3 components with micro/nano-particles: silica, bentonite or organic micropolymers.
- Non-ionic systems: PEO/cofactor (phenolic resin).

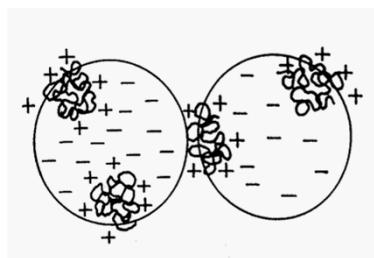


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25

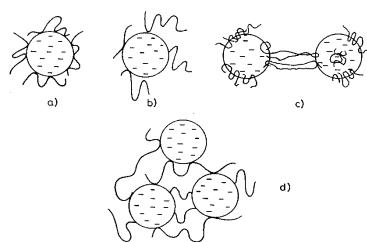


FLOC PROPERTIES



SOFT FLOCS

- Easy to break down
- Reflocculation
- More compact

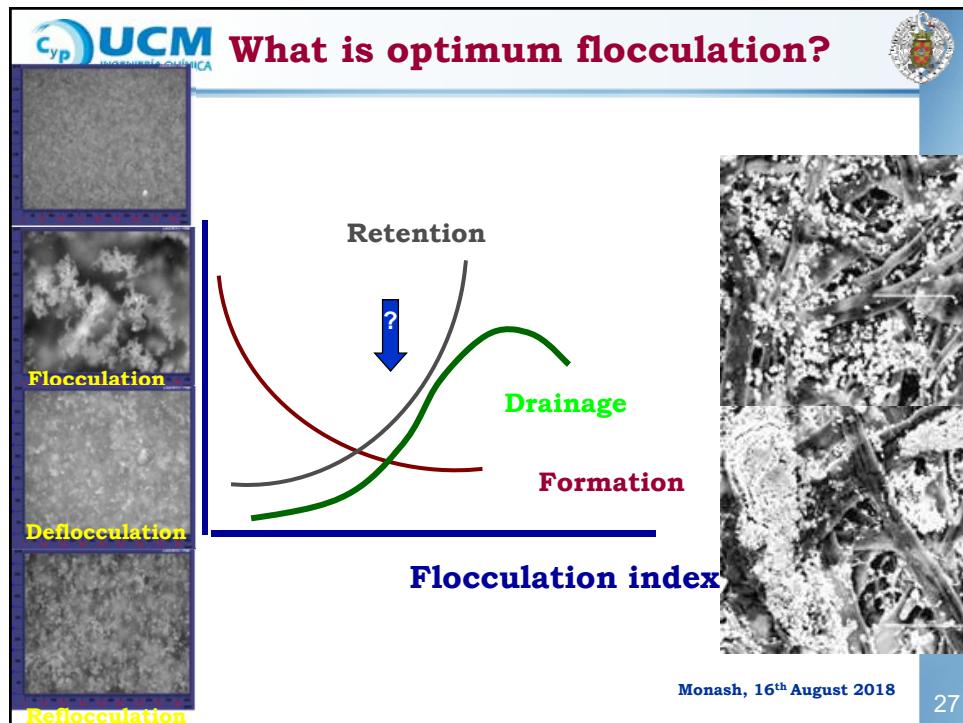


HARD FLOCS

- Difficult to break down
- Partial reflocculation
- More voluminous

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26



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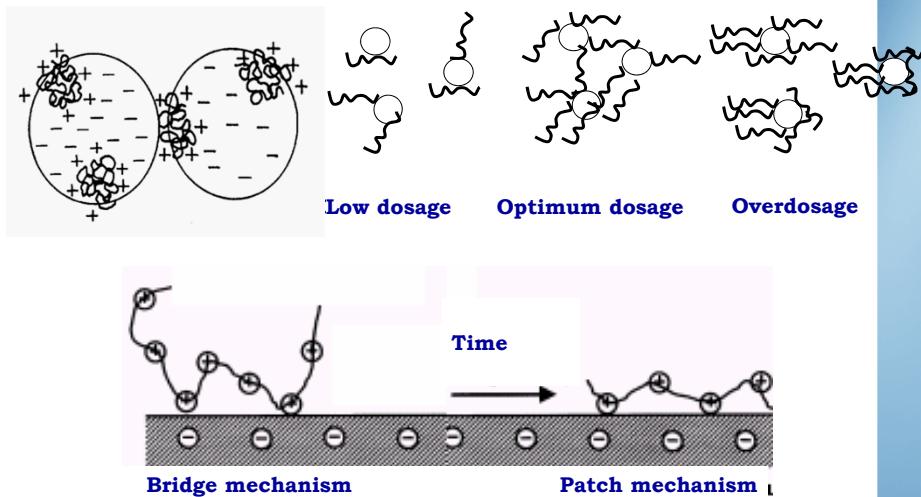
Cualitative relationships between flocs and papermaking processes

INFLUENCE	POSITIVE
PROCESS	
Drainage (foils)	Big and compact flocs
Drainage (vacuum)	Small and compact flocs
Drainage (press)	Soft flocs
Retention	Fiber-filler flocs
PRODUCT	
Formation	Small and compact flocs
Porosity	Small flocs
Strength	Small flocs

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28

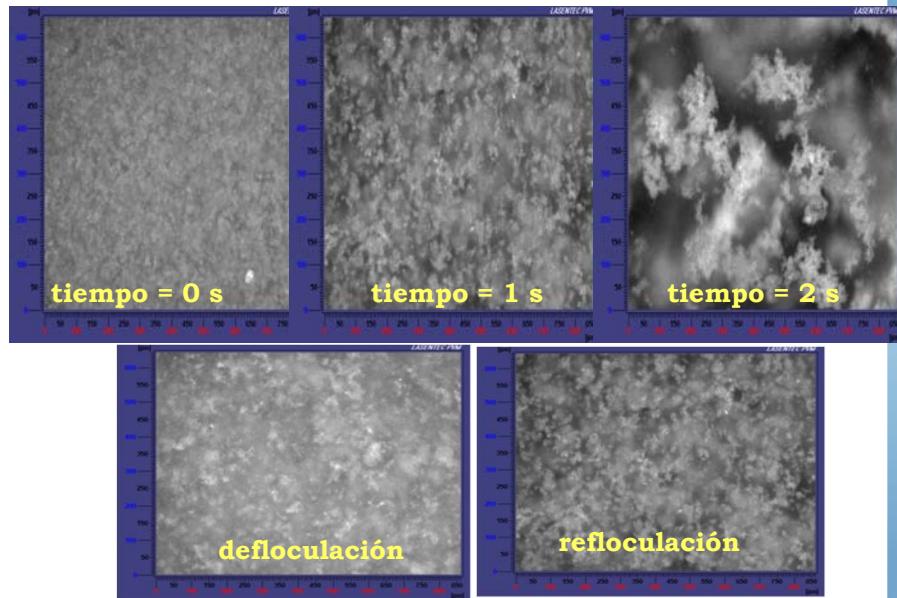
Effect of flocculant dosage & time

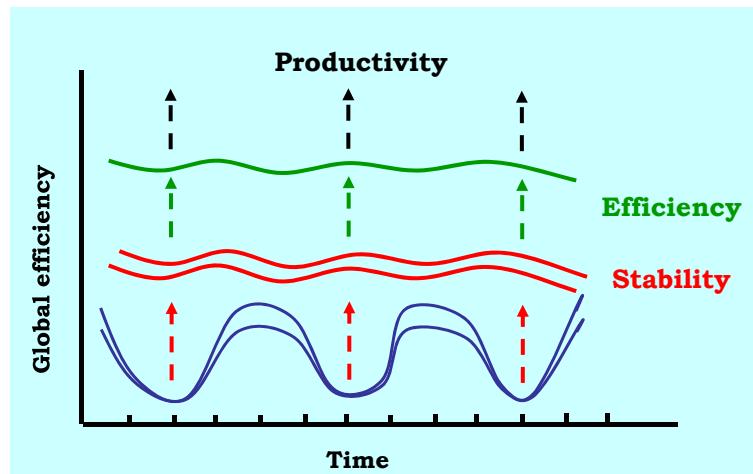


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29

Dosification point



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31



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32



1. HIGH PRODUCTIVITY

- Formation
- Retention
- Drainage



Max. production
Without breaks
Minimum cost



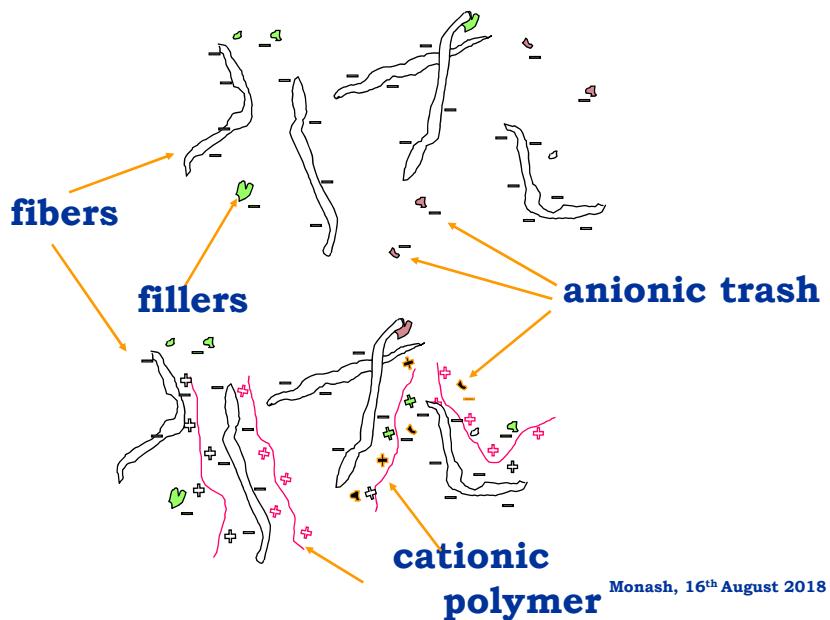
2. HIGH QUALITY PRODUCTS



Opacity, brightness, strength,

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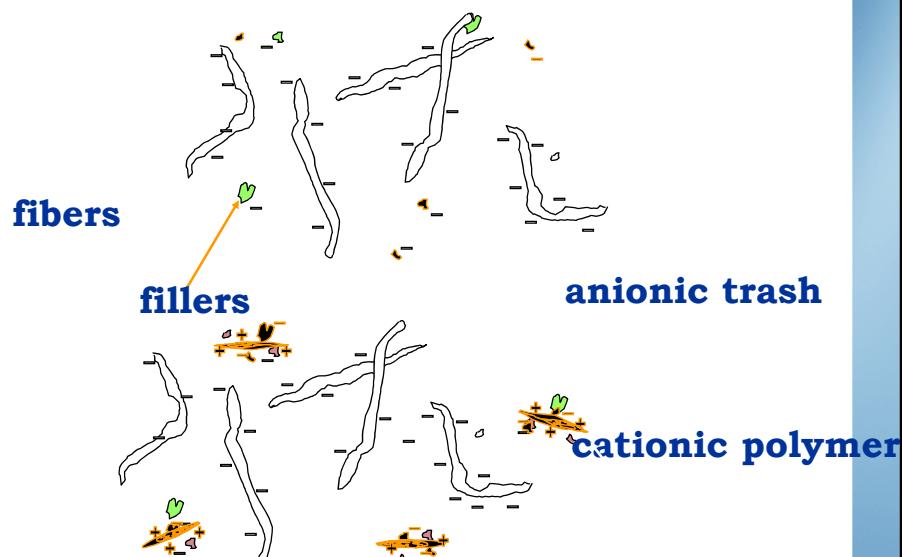
33



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34

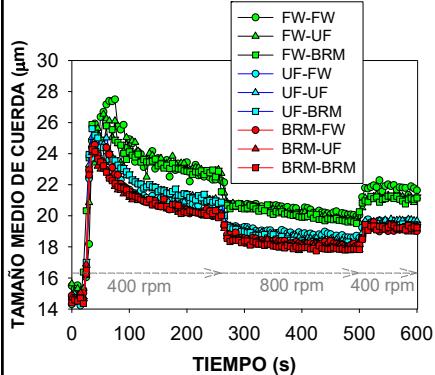
Competition for retention additives



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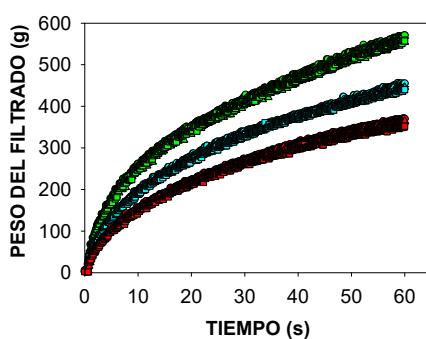
35

Water quality vs flocculation and drainage



FLOCCULATION

- Larger chord lengths with FW.
- Similar floc reversibility
- Bentonite ≠ f (water quality).

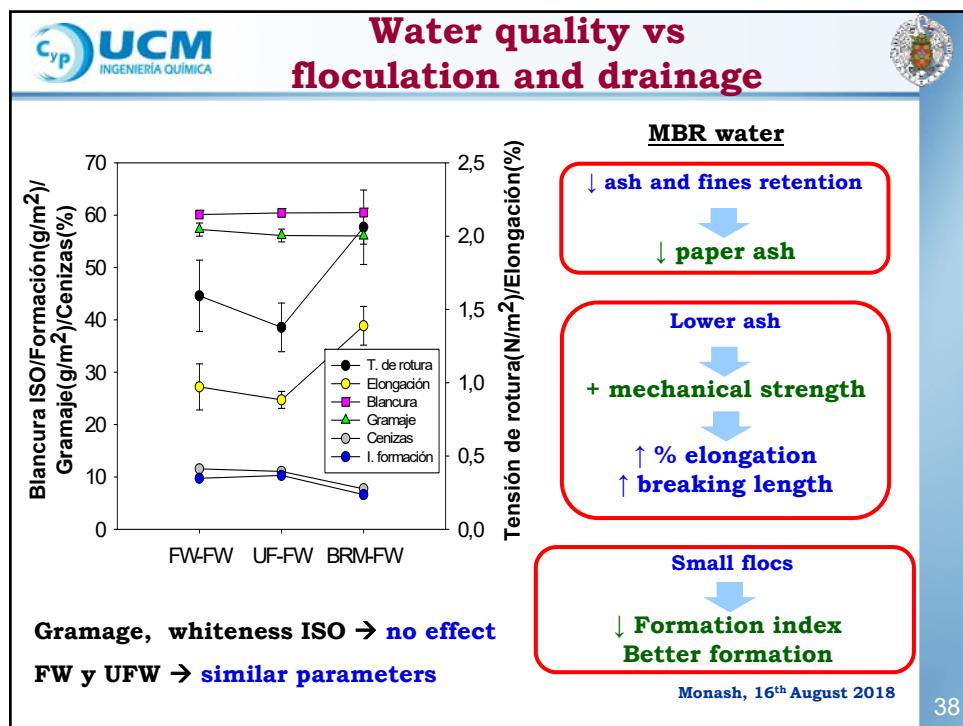
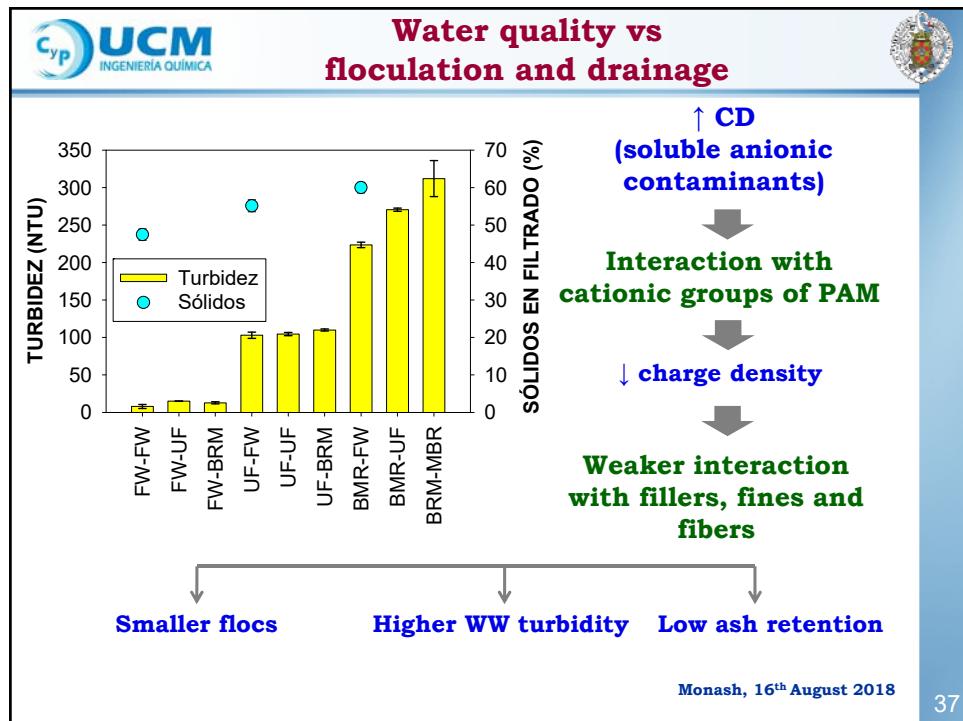


DRAINAGE

- Lower drainage time with FW.
- Bentonite ≠ f (water quality).

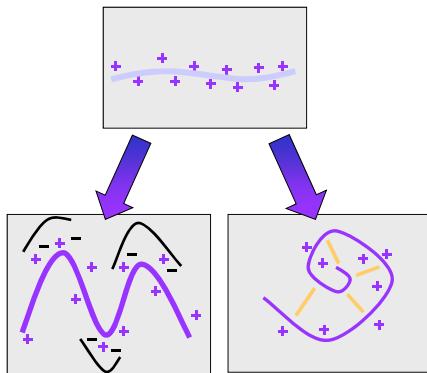
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36





Reduction of the additive efficiency



DCM agglomeration

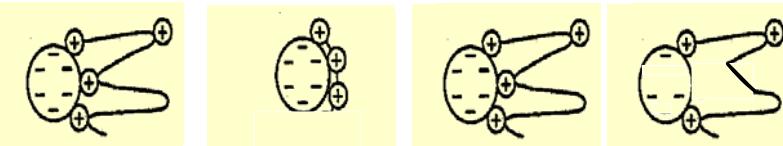
↓
DEPOSITS

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39



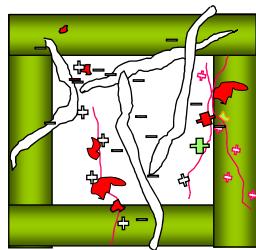
- If conductivity increases agglomeration is induced and the required dosages of flocculant decrease.
- Polymer conformation may change and flocculation mechanism shifts towards a charge model. The polymer is still effective but produce smaller flocs.
↓ Bridges ⇒ ↓ big flocs
- High ionic strength partially neutralise the polymer charge which reduced the adsorption of polymer and may affects the size of the flocs.



40

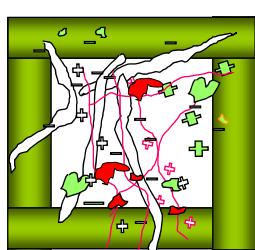


Low dosage
Cost: A1



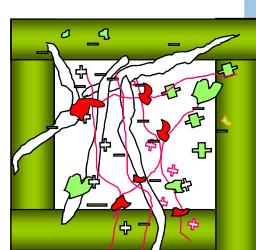
PZ ≈
DC of WW ↓
Retention ↓

High dosage
Cost: A2



PZ of pulp ↓
DC of WW ↓
Retention ↑

1.-Coagulant thick stock
2.-Ret. aid low dosage
Cost: C+A3



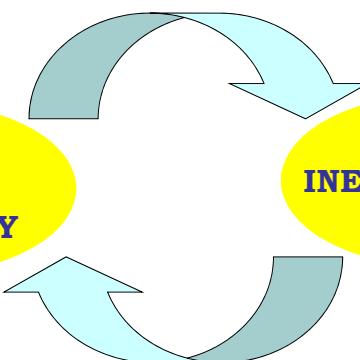
DC ↓ PZ ≈
DC ≈ PZ ↓
Retention ↑
Cost < A2

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41

**COMPLEX
WET END
CHEMISTRY**

INESTABILITIES



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43

Content

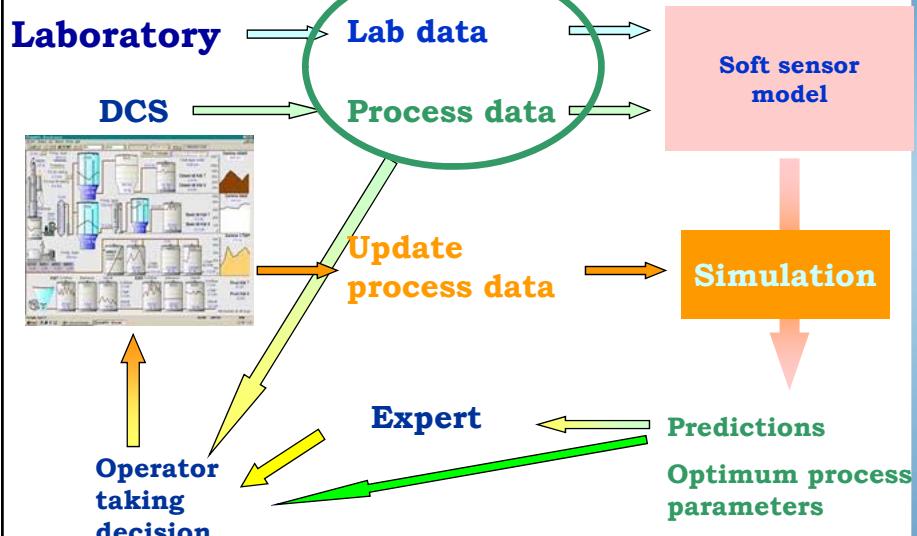


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44

On-line wet end control



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45

Wet end variables



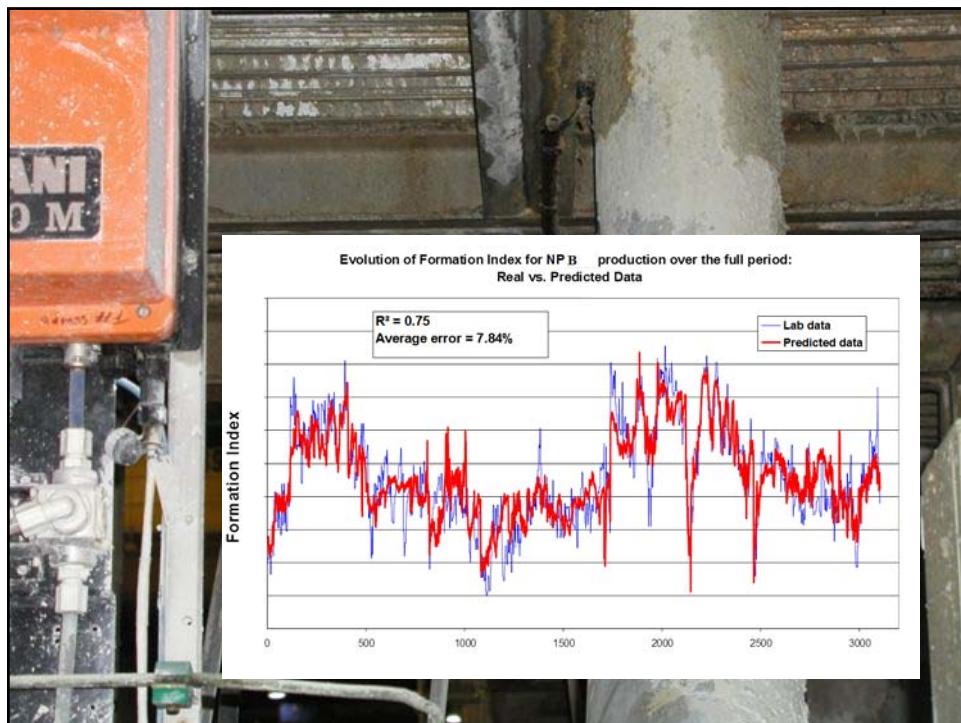
1. Objetivo
2. Procesos
3. Herramientas.
4. Metodolog
- 5b. Res.Papel
6. Conclus.

VARIABLE	UNIDS.
Gramaje (PaperLab) PM61	g/m ²
Espesor (PaperLab) PM61	μm
Indice Formación (PaperLab) PM61	
Rcia. Tracción (PaperLab) PM61	kN/m
Rcia. Desgarro (PaperLab) PM61	Nm ² /g
Elongación (PaperLab) PM61	
Densidad (PaperLab) PM61	kg/m ³
Hand (PaperLab) PM61	cm ³ /g
Longitud de rotura (PaperLab) PM61	km
Long. TEA (PaperLab) PM61	J/m ²
Longitudinal TSI (PaperLab) PM61	kNm/g
Transversal TSI (PaperLab) PM61	kNm/g
Porosidad (PaperLab) PM61	ml/min
Opacidad (PaperLab) PM61	%
Brillo (PaperLab) PM61	%
Humedad en parte final de PM61	%
Cenizas base en papel PM61	%
Cenizas en parte final de PM61	%
Humedad en Prensa Pivo	
cps (1-5 μm)	Cts/s
cps (5-34 μm)	Cts/s
cps (34-1000 μm)	Cts/s
Media, 1/Lin Pond.	μm
Media, Cuad. Pond.	μm
Mediana.	%
%<5.41	%
%>34.15	%

VARIABLE	UNIDS.
Cons. Caña Entrada (DCS) PM61	g/l
Cons. Caña Entrada (l/ah) PM61	%
Cenizas caja entrada (DCS) PM61	g/l
Cenizas caja entrada (Lab) PM61	%
Cons. Ag. Blancas (DCS) PM61	g/l
Cons. Ag. Blancas (Lab) PM61	%
Cenizas Ag. Blancas (DCS) PM61	g/l
Cenizas Ag. Blancas (Lab) PM61	%
Retención total (DCS) PM61	%
Retención total (Lab) PM61	%
Retención cenizas (DCS) PM61	%
Retención cenizas (Lab) PM61	%
Índice de flocculación PM61	
Destintado2 Caudal	m ³ /n
Destintado3 Caudal	m ³ /h
Caudal rotos	m ³ /h
Dosis floculante PM61	g/Ton
Dosis coagulante PM61	g/Ton
Dosis micropartícula PM61	g/Ton
Dosis CaCO ₃ PM61	l/n
Velocidad cable PM61	m/min
pH en PIT	

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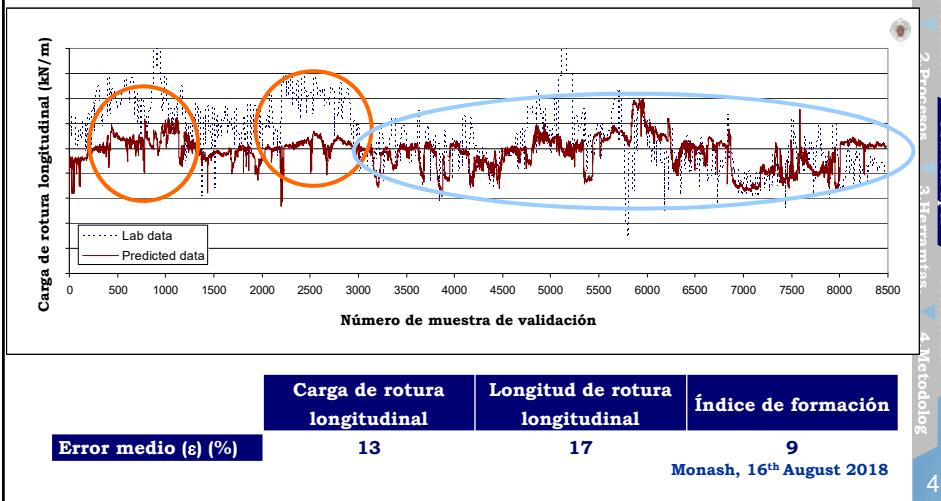
46



Predictions 3-6 months after model building



- Most of the production has the predicted data.
- Some periods have higher prediction error due to changes in the operating conditions.



1. Objetivo

5a.Res.Fibr.

2. Procesos

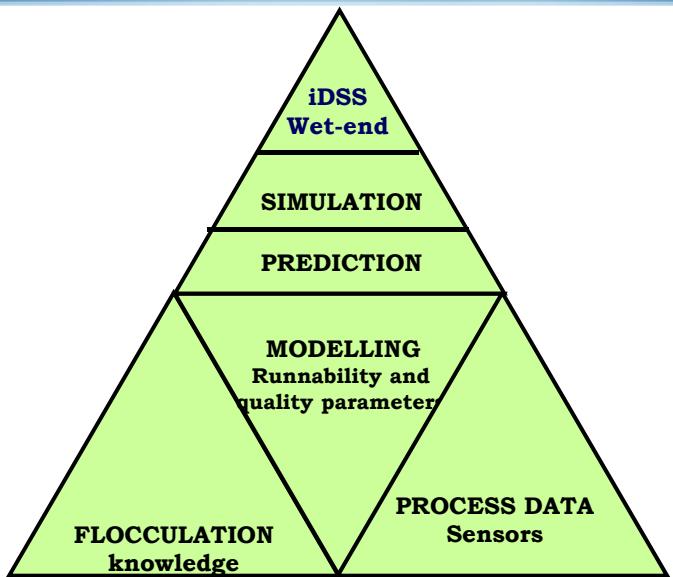
5b.Res.Papel

3.Herramientas

4.Metodolog

6.Conclus.

Wet-end vision



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50

Content



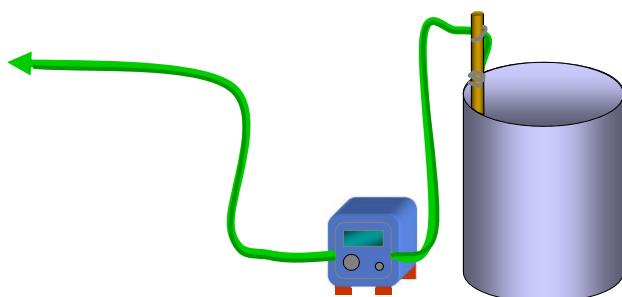
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51



WHICH ONE?
HOW MUCH?
WHERE?



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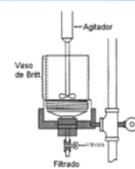
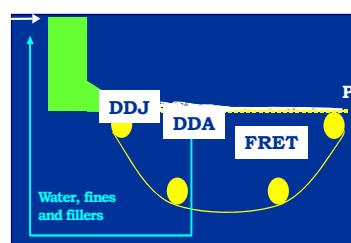
52

Wet-end audit methodology Retention-Drainage-Formation



RETENTION &
DRAINAGE
STUDIES

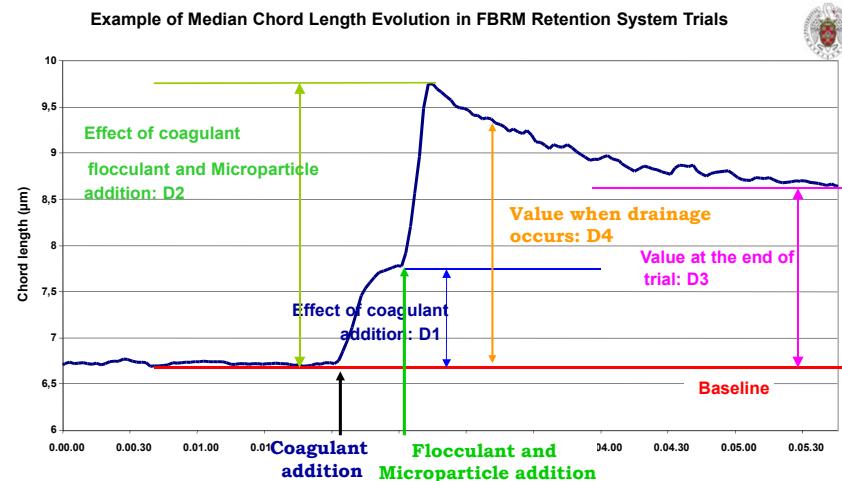
GRAVITY { DDJ
VACUUM { Dynamic drainage
 analyzer DDA
 Formation and
 retention tester (FRET)



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53

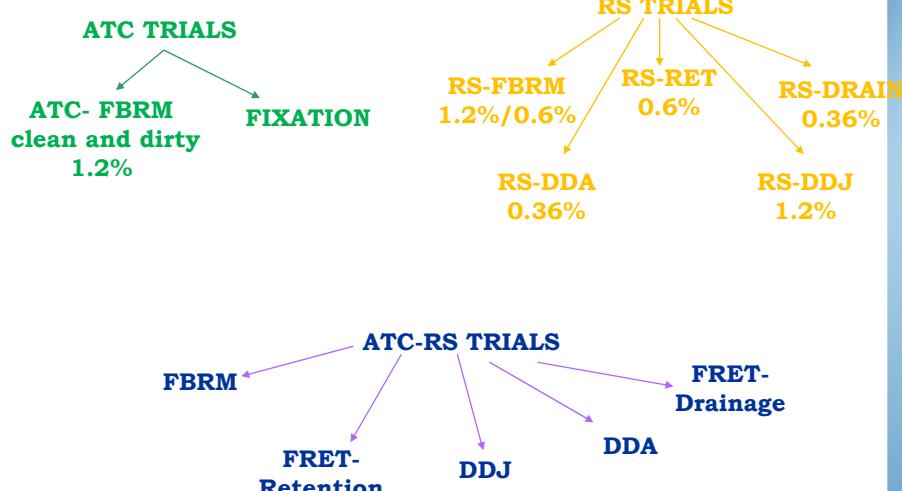
Wet-end methodology FBRM data



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54

Wet-end methodology





ATC-FBRM:

- Mean chord length
- Total counts/s
- > 58 µm evolution
- <5 µm evolution

RS-RET:

- Turbidity
- CD
- Gramage
- Total retention
- Ash retention
- Formation

RS-DDA:

- Drainage time
- Permeability
- Drainage curve
- Turbidity

RS-FBRM:

- Mean chord length
- Total counts/s
- >58 µm evolution
- <5 µm evolution

RS-DRAIN:

- Residual vacuum
- Total area
- Area > Tmax
- Total retention
- Ash retention
- Formation
- FBRM

RS-DDJ:

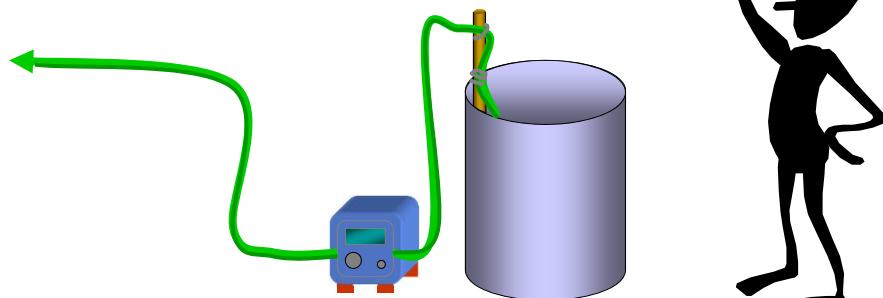
- Drainage time (100 mL)
- Turbidity
- Total retención
- Ash retención

Monash, 16th August 2018

56

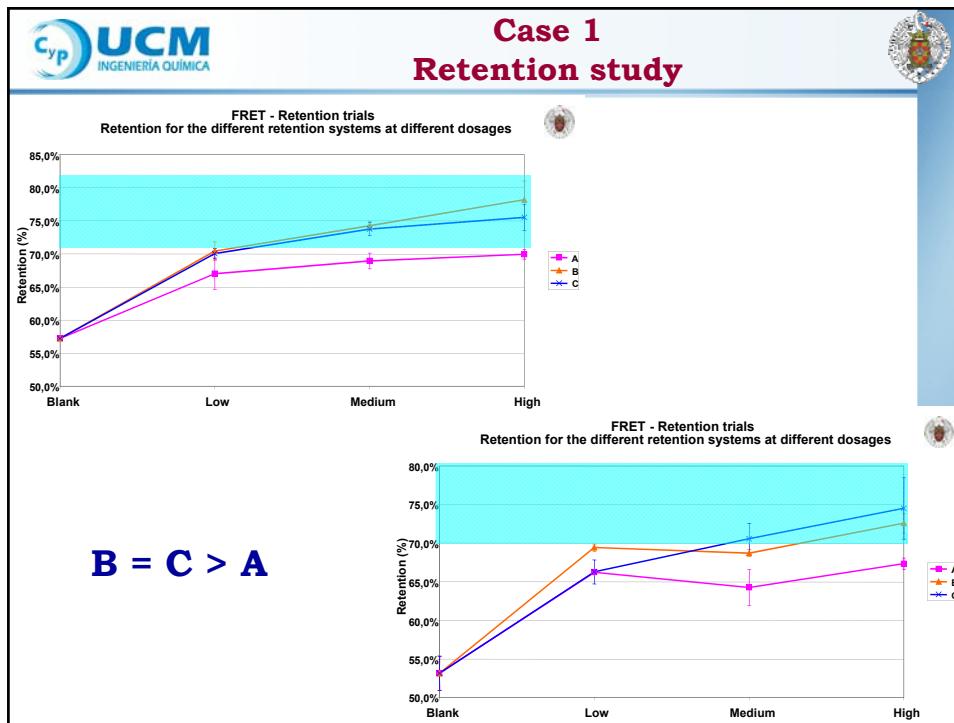


Which is the aim?



Monash, 16th August 2018

57



Case 2
Selection of retention systems

Trials Variable RS A RS B RS C Errors

18/05/04	Variable	RS A			RS B			RS C			Errors
		Dosage	Low	Medium	High	Low	Medium	High	Low	Medium	
RS DDJ	Drain Time	19.5	18.3	14.3	28.7	28.5	14.7	15.0	8.3	9.7	Low
	Turbidity	5943	3460	3910	4260	3485	1692	2379	2228	2992	Very Low
	Total Retention	89,4%	86,1%	85,6%	80,4%	84,1%	89,2%	90,2%	91,9%	89,6%	Medium
	Ash Retention	82,1%	77,1%	73,1%	71,0%	78,6%	80,7%	85,2%	85,0%	78,8%	Low
RS DDA	Drainage Time	-1	1	2	-1	-1	-1	-1	0	1	Very Low
	Permeability	0	-1	-1	0	0	0	1	0	0	High
	Turbidity	3480	2811	2413	2681	3120	1942	2889	2192	1807	Low
RS RET	CD	79,9	85,4	63,5	49,8	70,3	65,2	86,6	81,5	68,0	Low
	COD	411	415	392	393	413	426	412	406	444	Too High
	Grammage	53,04	51,65	54,18	55,48	56,02	58,20	53,25	56,55	59,68	Low
	Retention	66,2%	64,2%	67,3%	69,4%	68,7%	72,6%	66,3%	70,6%	74,5%	Low
	Form Index	27,37	24,75	21,63	26,05	25,13	20,53	27,40	23,73	20,73	Low
	HST DEV IF	5,68	6,33	7,02	5,78	6,10	7,48	5,57	6,44	7,24	Very Low
	Ash Content										Very Low
	V _{res}	108	133	104	172	143	134	173	157	138	Medium
RS DRAIN	Total area	1598	2043	1898	2315	2091	1947	2470	2231	1992	Low
	Area >Tmax	1454	1874	1734	2146	1928	1782	2299	2066	1834	Medium
	%Area >Tmax	91,0%	91,8%	91,3%	92,7%	92,2%	91,5%	93,1%	92,6%	92,1%	Low
	Grammage	54,36	52,55	50,81	58,87	53,06	57,43	57,79	61,09	57,91	High
	Total Retention	67,7%	65,0%	63,1%	73,1%	65,7%	72,1%	71,6%	76,3%	74,3%	Medium
	Form Index	25,9	34,5	35,9	26,1	29,5	28,0	24,6	23,8	26,8	Low
	HST DEV IF	6,3	4,5	4,2	5,7	5,2	5,5	6,1	6,6	5,6	Low
	Ash Content	24,5%	20,5%	21,9%	26,5%	23,9%	26,7%	27,9%			Very Low
	D2TM	2	6	7	4	5	5	2	3	8	Low
	D4TM	3,5	4,5	5,5	3	3,5	4		4,5	6,5	Very Low
RS FBRM	D4 FN	3,8	4,5	4,8	3,8	4	4,3	5	6	6	Very Low

Monash, 16th August 2018

59

Case 2 Selection of retention system



Trials	Variable	RS A			RS B			RS C			Errors
18/05/2004	Dosage	Low	Medium	High	Low	Medium	High	Low	Medium	High	
RS DDJ	Drain Time	19,5	18,3	14,3	28,7	28,5	14,7	15,0	8,3	9,7	Low
	Turbidity	5943	3460	3910	4260	3485	1692	2379	2228	2992	Very Low
RS DDA	Drainage Time	4,1	4,3	4,1	4,2	3,8	3,5	3,9	3,3	3	Very Low
	Turbidity	3480	2611	2413	2681	3120	1942	2889	2192	1807	Low
RS RET	Retention	66,2%	64,2%	67,3%	69,4%	68,7%	72,6%	66,3%	70,6%	74,5%	Low
	Form Index	27,37	24,75	21,63	26,05	25,13	20,53	27,40	23,73	20,73	Low
RS DRAIN	Area >Tmax	1454	1874	1734	2146	1928	1782	2299	2066	1834	Medium
	Total Retention	67,7%	65,0%	63,1%	73,1%	65,7%	72,1%	71,6%	76,3%	74,3%	Medium
	Form Index	25,9	34,5	35,9	26,1	29,5	28,0	24,6	23,8	26,8	Low
	Ash Content	24,5%	20,5%	21,9%	26,5%	23,9%	26,7%	27,9%	27,9%	27,9%	Very Low
	D2TM	2	6	7	4	5	5	2	3	8	Low
RS FBRM	D4TM	3,5	4,5	5,5	3	3,5	4	4,5	6,5	6,5	Very Low

 Good drainage and formation

 Good retention

Monash, 16th August 2018

60

Case 3 Wet end audit- Optimization of costs



Trials	Variable	RS A			RS B			RS C			Errors
31/05/2004	Dosage	Low	Medium	High	Low	Medium	High	Low	Medium	High	
RS DDJ	Drain Time	62	20	18	53	25	25	40	22	25	Medium
	Turbidity	4558	5105	3885	4485	4185	2932	3788	4800	3352	Very Low
RS DDA	Drainage Time	4,86	5,53	4,45	4,98	4,54	3,64	4,79	4,05	4,84	Low
	Turbidity	1808	1580	1638	1550	1623	1448	1543	1502	722	Low
RS RET	Turbidity	4130	3077	2548	2835	2327	1458	2689	2452	2068	Very Low
	Retention	67,0%	69,0%	70,0%	70,4%	74,2%	78,2%	70,0%	73,8%	75,5%	Low
	Form Index	32,4	29,87	26,2	32,3	27,97	24,73	32,2	27,87	26,5	Low
	Ash Retention	26,2%	28,9%	31,1%	29,5%	35,2%	41,0%	31,5%	35,0%	38,2%	Very Low
	Area >Tmax	2487	2525	2119	3064	2792	2553	2920	2658	2497	Medium
	Total Retention	74,3%	76,4%	78,6%	74,0%	73,8%	81,2%	76,8%	75,9%	81,1%	Low
	Form Index	28,63	27,5	23,55	34,4	30,4	24,3	31,27	30,57	27,43	Low
	Ash Retention	66,3%	71,7%	72,7%	56,6%	63,7%	80,4%	70,5%	73,8%	83,9%	Low
	RS FBRM	1,6	2,1	2,9	1,7	2	3	1,7	2,2	4	Very Low

 Good results

A cost study is required

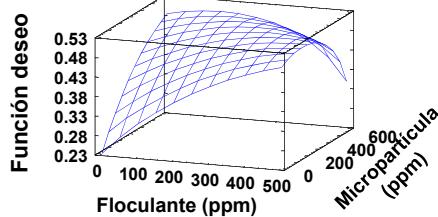
Monash, 16th August 2018

61

Case 3 Wet end audit- Optimization of costs



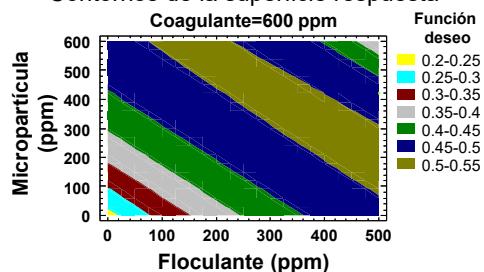
Superficie de respuesta estimada
Coagulante=600 ppm



Optimised variables:

- D2 maximum
- D3 maximum
- Minimum cost

Contornos de la superficie respuesta
Coagulante=600 ppm



Estimated optimum:

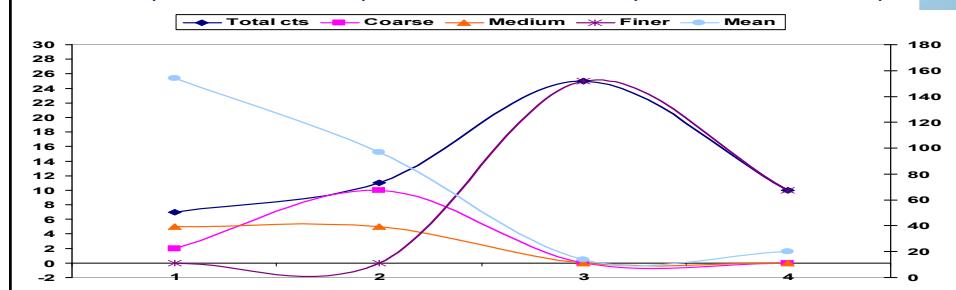
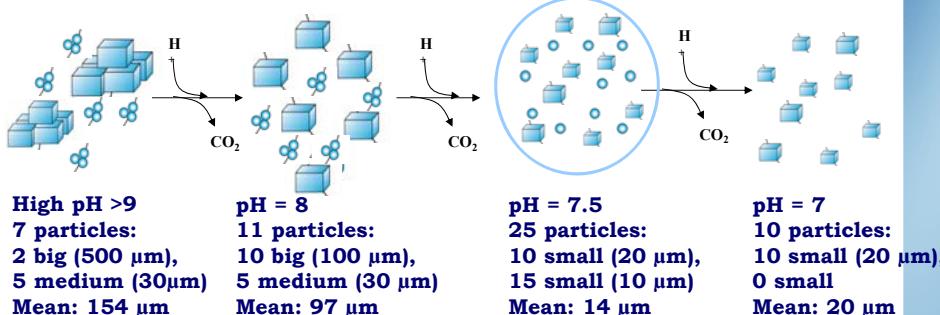
- Coagulant = 0 ppm
- Flocculant = 500 ppm
- Microparticle = 422 ppm

62

Case 4 Understanding pH effects



Lower Retention





WET END OPTIMIZATION SEMINAR

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14